

## **APPENDIX I**

### **Design Guidelines for Slope Tapered Box Culverts**

The purpose of slope tapered box culverts is to reduce construction costs by using a smaller barrel but still providing acceptable hydraulic capacity and upstream headwater. These special inlets have been used in Iowa and across the country since the 1950's or earlier. Successful use of these inlets requires careful hydraulic design and good construction practice.

The culvert site normally will meet two basic requirements to qualify for a tapered inlet. The first is that the additional design costs are offset by the reduction in construction costs. The second is that the site must have enough fall for the design to perform properly, typically at least six to eight feet.

The culvert inlet is made large enough to keep the depth of water at the entrance within allowable limits. The slope tapered section funnels the water down a steep slope as the culvert width decreases. The barrel section is designed to flow nearly full when carrying the design discharge. Generally, the outlet has a flume and basin for energy dissipation.

#### **Design Steps**

There are five basic steps for the hydraulic design a box culvert with a slope tapered inlet:

1. Determine the design discharge. Refer to [Appendix J](#) for guidance. The Iowa Runoff Chart may be used for rural watersheds draining 1280 acres (518 hectares) or less.
2. Determine the allowable depth of water at the inlet. Typically, the Iowa DOT allows one foot (0.3 m) of water above the top of the inlet.
3. Select an inlet size that results in a flow depth less than or equal to the allowable. Inlet control nomographs from FHWA's "Hydraulic Design of Highway Culverts," HDS No. 5, can be used for this.
4. Select a barrel size and slope that results in the barrel flowing less than full. The barrel height should be the same as the inlet, while the barrel width should generally be no less than 50 to 60% of the inlet width. Select a slope steep enough to maintain supercritical flow. Charts in FHWA's "Design Charts for Open-Channel Flow", HDS No. 3, have been developed from Manning's equation and can be used to select the appropriate slope.
5. Determine the drop and length of the slope tapered section. The minimum drop needed is the specific energy at the inlet ( $H_1$ ) minus the specific energy at the barrel ( $H_2$ ) plus energy losses ( $H_L$ ). Specific energy is the depth plus velocity head at a given location.

The following guidelines, charts and worksheets (English and metric units) are provided to assist in the hydraulic design.

When the inlet will be raised significantly to create a pond, geotechnical concerns must be considered to ensure that seepage through the embankment is not excessive.

### General Guidelines

1. HW from inlet control charts for proposed inlet size, no greater than  $D + 2$  ft (0.6 m).
2. The height (D) of the structure does not change.
3. Calculated Z may be rounded to the next higher increment as described below. Minimum Z = 3 ft. (0.9 m).
4. Taper can be designed by using the RCB standard reinforced steel pattern of inlet size for the entire length of the taper and varying the length of the transverse steel.
5. The barrel outlet flow line is usually set at least  $\frac{1}{2}$  (D) above streambed. This prevents the barrel from "drowning out".
6. The outlet usually has a flume with a basin that is buried 4 to 6 ft. (1.2 to 1.8 m) below streambed, to help dissipate energy.
7. The barrel slope ( $S_o$ ) should generally be 1.5% or steeper in order to maintain supercritical flow and the maximum flow depth of 0.9D in the barrel. See "Design Charts for Open Channel flow," HDS No. 3, FHWA, to determine specific flow depths for various slopes.
8. An attempt should be made to design barrel sizes to conform with standard RCB sizes. This may mean starting with a "wide" non-standard inlet.
9. Assume energy loss,  $H_L = 0.2$  ft. (0.1 m) for all cases.

### Guidelines for single RCBs

1. Use drop rate (L/Z) of approximately 3: 1.
2. Ratio of barrel width to inlet width ( $B_2/B_1$ ) should be 50% or greater.
3. For Z=3ft., use L=10ft. For Z=4ft., use L=12ft. For Z=5ft., use L=15ft.  
(For Z=0.9m, use L=3.0m. For Z=1.2m, use L=3.6m. For Z=1.5m, use L=4.5m)

### Guidelines for Twin RCBs

1. Use drop rate (L/Z) of 5:1 (min.).
2. Ratio of barrel width to inlet width ( $B_2/B_1$ ) should be 60% or greater.
3. L is determined either by  $(B_1 - B_2) \times 4$  or  $Z \times 5$ , whichever is greater. This insures a minimum side taper of 4:1. L should generally be in 5 ft. (1.5 m) increments.

### Definitions

HW = Headwater from inlet control charts

$H_1$  = Specific energy head at inlet

$H_2$  = Specific energy head at barrel

$B_1$  = Width of inlet opening

$B_2$  = Width of barrel opening

D = Height of opening

$H_L$  = Energy loss

$d_c$  = Critical depth

Z = Drop in flow line required

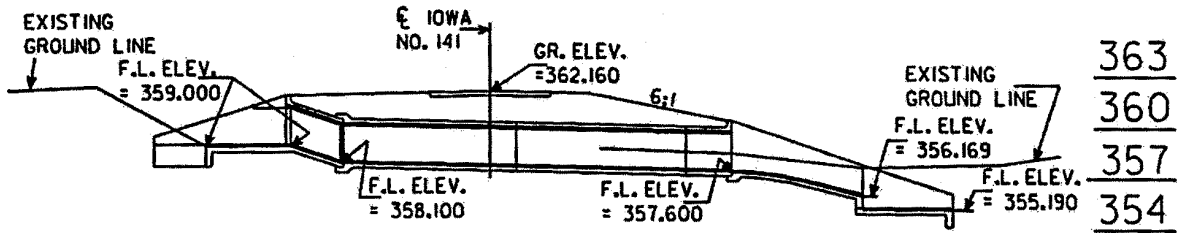
L = Length of taper section

$S_o$  = Slope of barrel

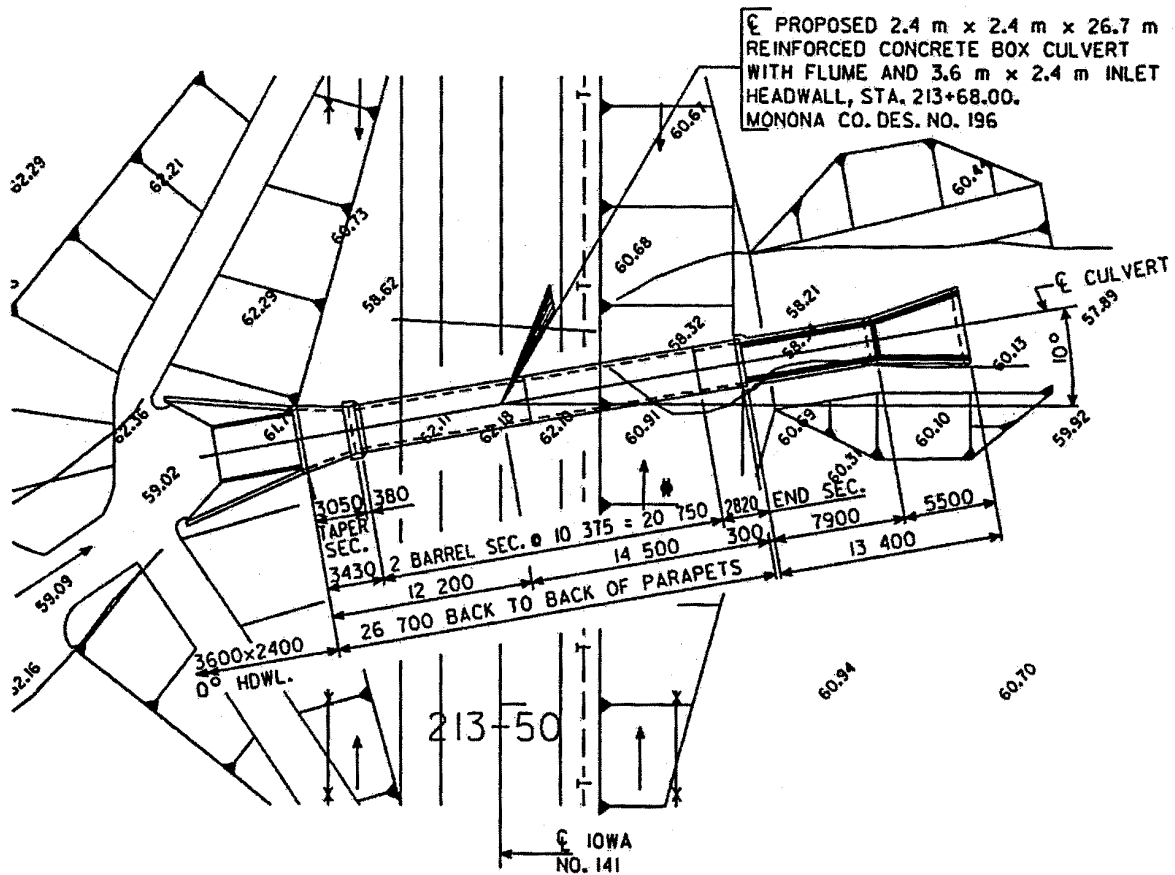
$V^2/2g$  = Velocity head

$N = L/Z$  = Slope of taper section

## Sample Slope Tapered Box Culvert and Flume

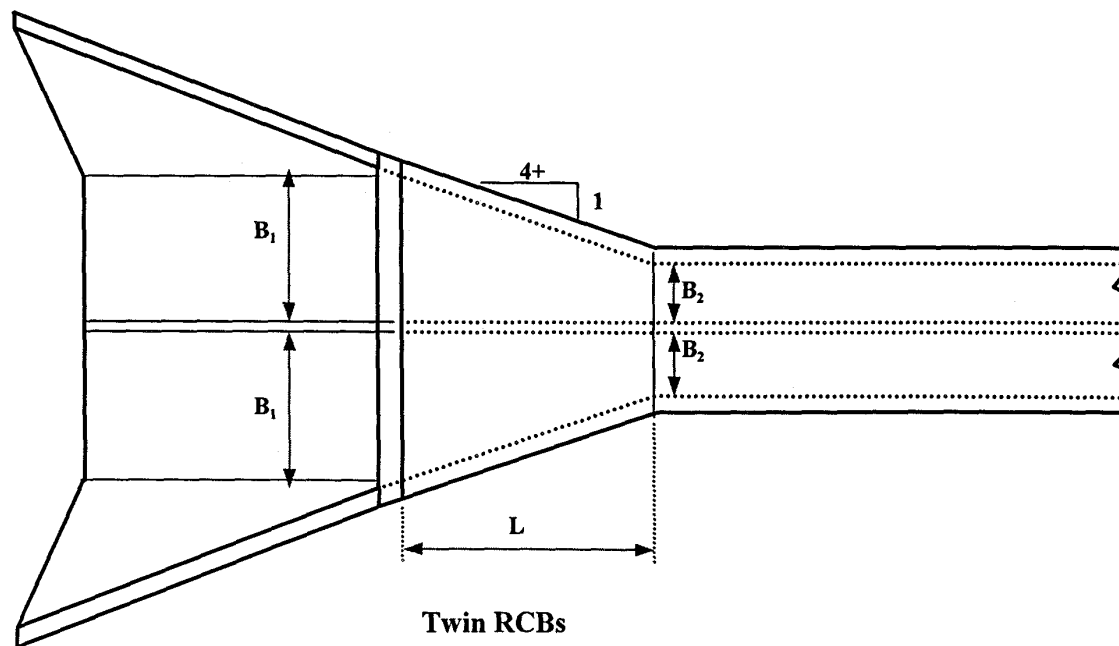
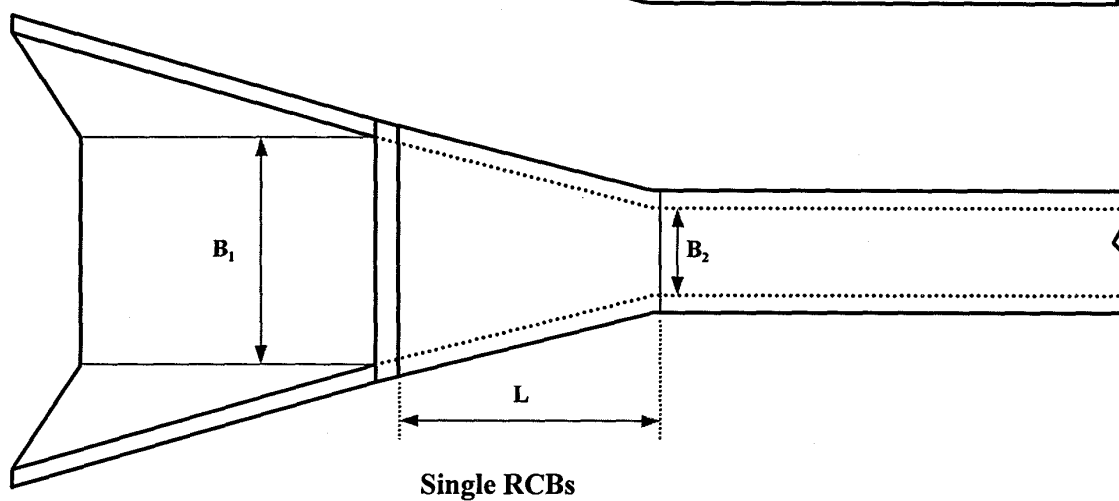
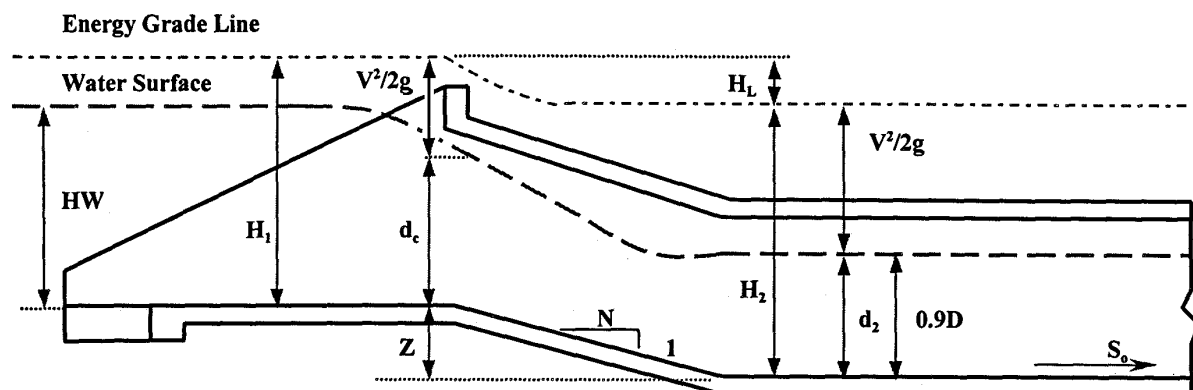


LONGITUDINAL SECTION ALONG  $\phi$  CULVERT



SITUATION PLAN

## Slope Tapered Box Culverts



### Worksheet for Slope Tapered Box Culverts (English)

Project \_\_\_\_\_ County \_\_\_\_\_ Date \_\_\_\_\_  
Station \_\_\_\_\_ Designer \_\_\_\_\_

| Variable   | Example | Trial 1 | Trial 2 | Trial 3 | Trial 4 |
|--|---------|---------|---------|---------|---------|
| Design Q, ft <sup>3</sup> /sec                               | 600     |         |         |         |         |
| <b>Inlet Section</b>   |         |         |         |         |         |
| B <sub>1</sub> x D, ft. x ft. (size of inlet)                | 10 x 6  |         |         |         |         |
| Q/ B <sub>1</sub>  | 60      |         |         |         |         |
| HW, ft. (from HDS No. 5 nomographs)                          | 7.5     |         |         |         |         |
| d <sub>c</sub> , ft. (from design graph)                     | 4.8     |         |         |         |         |
| H <sub>1</sub> , ft. (from design graph)                     | 7.2     |         |         |         |         |
| <b>Barrel Section</b>  |         |         |         |         |         |
| B <sub>2</sub> x D, ft. x ft. (size of barrel)               | 6 x 6   |         |         |         |         |
| Q/ B <sub>2</sub>  | 100     |         |         |         |         |
| 0.9 x D, ft.   | 5.4     |         |         |         |         |
| H <sub>2</sub> , ft. (from design graph)                     | 10.7    |         |         |         |         |
| <b>Slope Tapered Section</b>                                 |         |         |         |         |         |
| H <sub>L</sub> , ft. (assumed)                               | 0.2     | 0.2     | 0.2     | 0.2     | 0.2     |
| Z, ft. (= H <sub>2</sub> - H <sub>1</sub> + H <sub>L</sub> ) | 3.7     |         |         |         |         |
| Selected Z, ft.  | 4.0     |         |         |         |         |
| Selected L, ft.  | 12      |         |         |         |         |
| <b>Barrel Slope</b>  |         |         |         |         |         |
| d <sub>n</sub> = 0.9 x D, ft.                                | 5.4     |         |         |         |         |
| Min. slope, % (from HDS No. 3 or Manning's eqn.)             | 1.5     |         |         |         |         |
| <b>Is the design acceptable?</b>                             | Yes     |         |         |         |         |